

EVALUATION OF CURING METHODS AND PERIWINKLE SHELL CONCRETE USING RESPONSE SURFACE METHODOLOGY

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ABSTRACT

The effects of periwinkle shell, curing duration and methods of curing on the compressive strength of concrete using response surface methodology were evaluated. However, the periwinkle shells were added to the concrete at 5%, 10% and 15% dosage by weight as partial replacement to the coarse aggregate. The concrete were cast at 0.5 w/c ratio and cured between 7 days and 28 days in both water and air. Regression equations relating the blended concrete compressive strength with both the curing duration and periwinkle shell were developed.

The results show that the water cured periwinkle blended concrete gave a better compressive strength than the air cured blended concrete at 5% replacement, with a 22.1% increase in the compressive strength. The adjusted R^2 of 0.9516 and 0.6838 for both water and air cured periwinkle concrete reveal that 95.16% and 68.38% of the systematic variations in the compressive strength of the periwinkle concrete is accounted for by the independent variables.

Keywords: blended concrete, curing duration, periwinkle shell, regression

1.1 INTRODUCTION

Concrete is one of the most used materials in building and civil engineering construction work. It's a composite material comprising of a binding course e.g cement, fine (sand) and coarse (gravel or crushed stones) aggregate. (Oyenuga, 2005). Fine aggregate is sand having particle size distribution not greater than 4.75mm in size while coarse aggregate is natural gravel or crushed stone usually larger than 4.75 mm and usually less than 16 mm in ordinary structure (Abede and Manasseh, 2009). It is worth stressing that coarse aggregate usually takes about 60% of the overall self-weight of normal weight concrete, thereby determining the quantity of reinforcement required to resist forces acting on the structural member (Adewuyi and Adegoke, 2008).

Periwinkles (*Nodilittorina radiata*) are small greenish blue marine snails with spiral conical shell and round aperture. Periwinkle shells are obtained from periwinkle. The hard shell periwinkles are now being considered as coarse aggregate in partial

replacement for expensive, unaffordable or unavailable crushed stones. Dahunsi 2003 reported that the main species of *Tympanostomus spp.* and *Pachmellania spp* are obtainable in some parts of Nigeria's Niger Delta, between Calabar in the east and Badagry in the west which have accumulated over the years in the southern part of the country. The periwinkle shells have been used mainly for light constructions. Different curing methods are usually adopted to evaluate the compressive strength of concrete. The methods include; water curing (pounding or immersion, sprinkling or fogging and saturated wet covering), dry air curing (self curing), and water retaining techniques (polythene sheet, formwork protection and curing compounds).

When cement touches water, it forms a paste which coats the surface of the fine and coarse aggregates. This paste hardens through hydration process to form concrete, and their property depends upon many factors including the quality and proportions of the ingredients and the curing environment. The most important indicator of the above properties is the water/cement ratio and the major properties of concrete influenced by water are workability, porosity, permeability and strength (Olafusi and Olutoge, 2012). Factors influencing compressive strength characteristics are cement characteristics, proportions of aggregates, water/cement ratio, degree of compaction efficiency of curing and temperature during curing period (Neville, 1993; Rusinoff, 1998). The adoption of right curing method for the periwinkle shell concrete may determine how best it can be used in the construction industry.

Some researchers lately have found interest in the use of periwinkle shells in concrete due to its availability especially in the riverine areas. Abede and Manasseh (2009) studied the suitability of periwinkle shell as partial replacement for river sand in concrete. They reported that concrete mixes of 0:1, 1:3, 1:1 and 1:3 Periwinkle-gravel can be classified as normal weight concrete, while those of 1:0 concrete mix of periwinkle-gravel are lightweight concrete. Adewuyi and Adegoke (2008) examined the exploratory study of periwinkle shells as coarse aggregate in concrete works. They observed that 35.4% and 42.5% of the periwinkle shell in replacement for granite was quite satisfactory for compressive strength when using concrete mix ratios of 1:2:4 and 1:3:6 respectively. Otunyo et al. (2013) examined the exploratory study of crushed periwinkle shell as partial replacement for fine aggregate in concrete. They found out that 50% of periwinkle shells can be added to 1:2:4 concrete mix as replacement for fine aggregate to give a compressive strength of 18 N/mm² which falls under lightweight concrete according to ASTM C330 (2017).

Oyedepo (2016) studied the evaluation of the properties of lightweight concrete using periwinkle shells as a partial replacement for coarse aggregate. He reported that the optimum compressive strength of 16.79 N/mm² and 16.71 N/mm² at 20% and 30% replacement was suitable for lightweight concrete according to ASTM C330 (2017). Osayemwen (1992) examined the utilization of periwinkle shells as alternative material to granite chips as coarse aggregate in concrete and concluded that the use of periwinkle shells for concrete would result in low cost housing delivery especially in the riverine areas where they are found as waste. The concrete produced with these periwinkle shells are light weight concretes required for non load bearing walls, non structural floors, strip footing and other non structural elements (Falade, 1995).

Periwinkle shells as partial replacement for crushed granites would go a long way reducing the cost of construction especially in areas where light weight concrete is required. This study tends to unravel the potentiality in periwinkle shell being used as partial replacement for coarse aggregate in concrete and also to ascertain the best curing methods that would be adopted for coastal areas where periwinkle shells are readily available using response surface methodology.

2.1 MATERIALS AND METHOD

The material used includes Portland cement, 20mm size of crushed coarse aggregate, fine aggregate, periwinkle shell and water. The tools include steel moulds (100mm x 100mm x 100mm size), shovel and head pans. The periwinkle shells were washed to remove impurities and dried before usage in the designs mix of 20 N/mm² concrete adopted. The periwinkle shells were partially replacement for 5%, 10% and 15% respectively using 0.5 water/cement ratios. Fifty six (56) cubes of 100 mm x 100 mm x 100 mm with two cubes were made for each mix in accordance with BS 1881: 102 (1983). However, the concrete were cast and cured between 7 days and 28 days both in water and air respectively.

Design expert software was used to produce the experimental design for the periwinkle concrete as shown in Table 1.0. The coded value of 5% to 15% for the periwinkle shell and 7 days to 28 days for the curing duration for both air and water curing methods were used. These produced thirteen factorial designs which was performed using grade 20 concrete and the responses were obtained as stated in Table 2.0.

Table 1.0: Experimental design matrix for the factorial design value for the blended concrete cured with both water and air

Experiment	Independent Variable	
	Periwinkle shell (%)	Curing duration (days)
1	10	17.5
2	10	17.5
3	15	28
4	10	5
5	5	28
6	15	7
7	10	28
8	15	17.5
9	10	17.5
10	10	17.5
11	5	7
12	10	17.5
13	5	17.5

The regression equations relating the compressive strength of the blended concrete with both the curing durations and percentages of periwinkle ash were developed using a commercial statistical package, Design-Expert Software 7.0.0. (Stat-Ease Inc., Minneapolis, USA). Response Surface Methodology (RSM) using the Central Composite Design (CCD) was applied to study the response (compressive strength of the blended concrete) on the independent variables (curing duration and percentages of periwinkle ash in the concrete). The regression coefficient of the linear model was determined using data obtained from the central composite design employed for the optimization of the independent variables as shown in Equation (1.0)

$$y = b_0 + \sum_{i=1}^n b_i x_i + \sum_{i=1}^n b_{ii} x_i^2 + \sum_{ii>j}^n \sum_j^n b_{ij} x_i x_j + e \quad (1.0)$$

where;

$$y =$$

predicted response (compressive strength of blended concrete)

b_0, b_i, b_{ii}, b_{ij} = coefficients

n = number of independent variables

x_i, x_j = actual factors

e = error term

F-test was used to evaluate the significant of the model while the adequacy of the model was checked using the coefficient of determination R^2 and adjusted R^2

3.1 RESULTS AND DISCUSSION

Regression equations relating the compressive strength of the blended concrete with both the curing duration and periwinkle shell were developed. The suitability of these equations was tested using the analysis of variance (ANOVA).

Multiple regression analysis was applied on the data in Table 2.0. The regression analysis was fitted to the polynomial in equation 1.0 and equation 2.0 and equation 3.0 were generated in terms of the actual factors for the compressive strengths for both water and air cured blended concrete. ANOVA for the linear model equations were carried out for the blended concrete and the results are presented in Table 3.0 and Table 4.0

$$cs_w = 29.54422 - 0.75355ps_a + 0.29137cu_d \quad (2.0)$$

$$cs_a = 26.18757 - 0.65506ps_a + 0.27261cu_d \quad (3.0)$$

where;

cs_w = compressive strength obtained when cured in water

cs_a = compressive strength obtained when cured in air

ps_a = periwinkle shell percentage

cu_d = curing duration in days

According to Table .0, the adjusted R^2 of 0.9516 shows that 95.16% of the systematic variations in the compressive strength of the concrete is accounted for by the independent variables (periwinkle shell percentage and curing duration). The F-value of 118.95 is statistically significant which indicates that the linear model can help us to predict the compressive strength of the concrete when cured in water.

Furthermore, Table 4.0 shows ANOVA for the linear model of the blended concrete cured in air. The adjusted R^2 of 0.6838 reveals that 68.38% of the systematic variations in the compressive strength of the blended concrete are accounted for by the independent variables (periwinkle shell percentage and curing duration). The F- value of 13.95 is statistically significant which indicates that the linear model can help us to predict the compressive strength of the concrete when cured in air.

Table 2.0: Experimental design matrix for the factorial design and response value for the blended concrete cured with both water and air

Experiment	Independent Variable		Response 1 (water)	Response 2 (air)
	Periwinkle shell (%)	Curing duration (days)	compressive strength (N/mm ²)	compressive strength (N/mm ²)
1	10	17.5	26.7	25.5
2	10	17.5	26.7	25.5
3	15	28	27.5	22.0
4	10	5	23.3	22.5
5	5	28	34.8	28.5
6	15	7	19.3	13.0
7	10	28	30.0	29.5
8	15	17.5	23.0	22.0
9	10	17.5	26.7	25.5
10	10	17.5	26.7	25.5
11	5	7	28.0	24.5
12	10	17.5	26.7	25.5
13	5	17.5	33.0	27.8

Table 3.0: Analysis of Variance for Linear Model Values of Blended Concrete Cured in Water

Source	Sum of Squares	Degree of Freedom	Mean Squares	F value	p-value Prob >F	
Model	188.45	2	94.22	118.95	< 0.0001	Significant
A- periwinkle shell	113.57	1	113.57	143.38	< 0.0001	
B- curing duration	74.88	1	74.88	94.53	< 0.0001	
Residuals	7.92	10	0.79			

Lack of fit	7.92	6	1.32			
Pure error	0.0	4	0.000			
Cor total	196.37	12				
CV= 3.35%	R ² = 0.9597	Adj R ² =0.9516	Pred R ² =0.9153			

3.2 DISCUSSION

3.2.1 Effect of Curing Duration and Periwinkle Shell Ash Percentage on the Compressive Strength of Concrete when Cured in Water

The three-dimensional plots of the combined effect of both the age of curing and periwinkle shell percentages on the compressive strength of concrete are shown in Figure 1.0. Increasing the age of curing of the concrete, increases the compressive strength. While increasing also the periwinkle shell dosage on the concrete, decreases the compressive strength. When the age of curing of concrete was 28 days at 5% periwinkle shell dosage, the maximum compressive strength of 34.8N/mm² was attained. This is 74% increase in compressive strength over the control concrete of 20 N/mm². However, maximizing both curing duration and periwinkle shell percentages gave 27.5N/mm² compressive strength for the blended concrete.

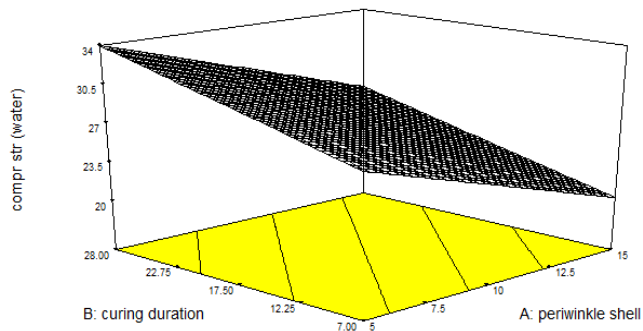


Figure 1.0: Combined effect of age of curing and periwinkle shell percentage on the compressive strength of the blended concrete cured in water

Table 4.0: Analysis of Variance for Linear Model Values of Blended Concrete Cured in Air

Source	Sum of Squares	Degree of Freedom	Mean Squares	F value	p-value Prob >F	
Model	151.37	2	75.68	13.95	< 0.0013	significant
A- periwinkle shell ash	85.82	1	85.82	15.85	< 0.0026	
B- curing duration	65.55	1	65.55	12.10	< 0.0059	
Residuals	54.16	10	5.42			
Lack of fit	54.16	6	9.03			
Pure error	0.000	4	0.000			

Cor total	205.53	12				
CV=	R ² =	Adj	Pred			
3.35%	0.7365	R ² =0.6838	R ² =0.4483			

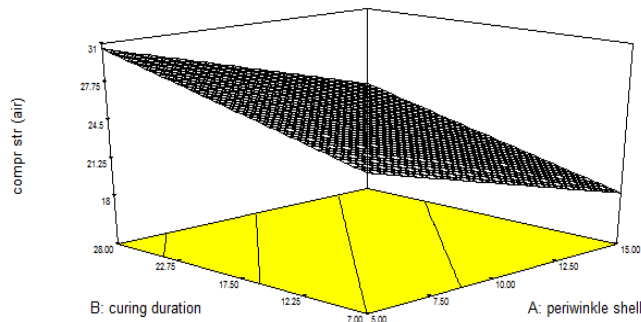


Figure 2.0: Combined effect of age of curing and periwinkle shell percentage on the compressive strength of the blended concrete cured in air

3.2.2 Effect of Curing Duration and Periwinkle Shell Percentage on the Compressive Strength of Concrete when Cured in Air

The three-dimensional plots of the combined effect of both the age of curing and periwinkle shell percentages on the compressive strength of concrete are shown in Figure 2.0. Increasing the age of curing of the concrete, increases the compressive strength. While increasing also the periwinkle dosage on the concrete, decreases the compressive strength. Maximising the compressive strength of the blended concrete and minimizing both periwinkle shell dosage and curing duration gave a compressive strength of 24.5N/mm². The optimum compressive strength of 29.5N/mm² was achieved at 10% periwinkle shell dosage and 28 days air curing duration. This is 47.5% increase in compressive strength over the control concrete of 20 N/mm².

4.1 CONCLUSION

It can be concluded from the study that:

1. The blended concrete gained strength with age upon curing irrespective of the curing method adopted.
2. The optimum compressive strength of 29.5N/mm² was achieved at 10% periwinkle shell dosage and 28 days curing duration when cured in air.
3. When the age of curing of concrete was 28 days at 5% periwinkle shell dosage, the maximum compressive strength of 34.8N/mm² was attained, when cured in water.
4. Curing method adopted affects the compressive strength of the blended concrete.
5. Water curing is the best curing method when compared to air curing because it increases the compressive strength by 22.1%
6. The results show that partial replacement with periwinkle shells up to 15% is possible in concrete since its compressive strength is still above the specified strength of 20 N/mm² at 28 days.

7. The Linear model was able to predict the compressive strength of the blended concrete with an adjusted coefficient of determination (R^2) of 0.9516 and 0.6838 for both water and air cured blended concrete.
8. This work has provided a data base for the use of periwinkle shell as partial replacement for coarse aggregate in grade 20 concrete.

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